

Vacuum System of SPS-II: Challenges of Conventional Technology in Thailand New Generation Light Source



Thanapong Phimsen

On behalf of SPS-II working groups





Siam Photon Source II (SPS-II)

- **High-energy and high-intensity synchrotron light source**
- *Located at the Eastern Economic Corridor (EEC) area in the EECi (EEC of innovation) district*
- *Aim to strengthen scientific community in both **academic and industrial research***
- **Scientific opportunities:** *Biomedical research, food and agriculture, industrial catalyst, advanced materials, environment, microelectronics and spintronics and archaeology and paleontology*
- *Currently in the design and prototyping stage – **plan for opening to users in 2029***

SPS VS SPS-II

Comparison of Technical Specification between SPS and SPS-II Machine

| | SPS-I | SPS-II | Advantage of SPS-II over SPS-I |
|---|---------------------------------------|---|---|
| Electron Energy | 1.2 GeV | 3.0 GeV | Higher Energy of Hard X-ray Photon |
| Beam current (max) | 150 mA | 300 mA | Larger Intensity of Synchrotron Radiation |
| Lattice Structure | DBA <i>Double Bending Achromat</i> | DTBA <i>Double Triple Bending Achromat</i> | Lower Electron Emittance |
| Operation Mode | Decade | Top-Up | Constant Photon Beam Brightness |
| Circumference | 81.3 m | 327.5 m | Greater Operational Flexibility |
| No. of IDs beamline (for Insertion / Straight Session) | 4/8 | 21/28 | More IDs for Beamline |
| Emittance | 60.5 nm·rad | < 1 nm nm·rad | Higher Brilliance |

Challenges

Local manufacturing technology

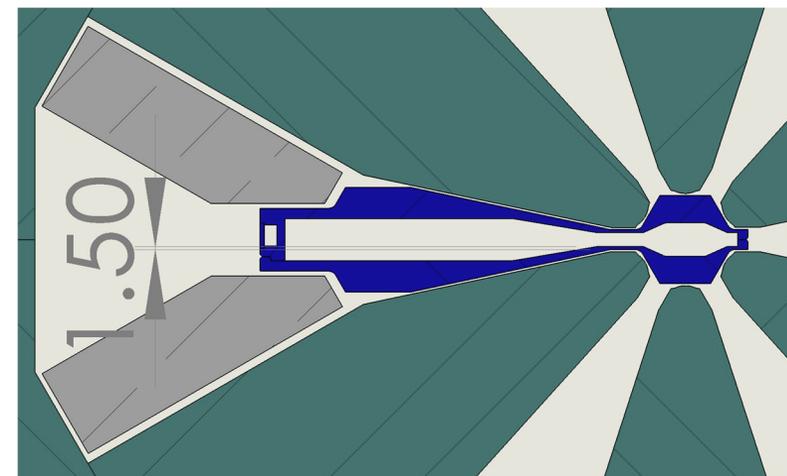
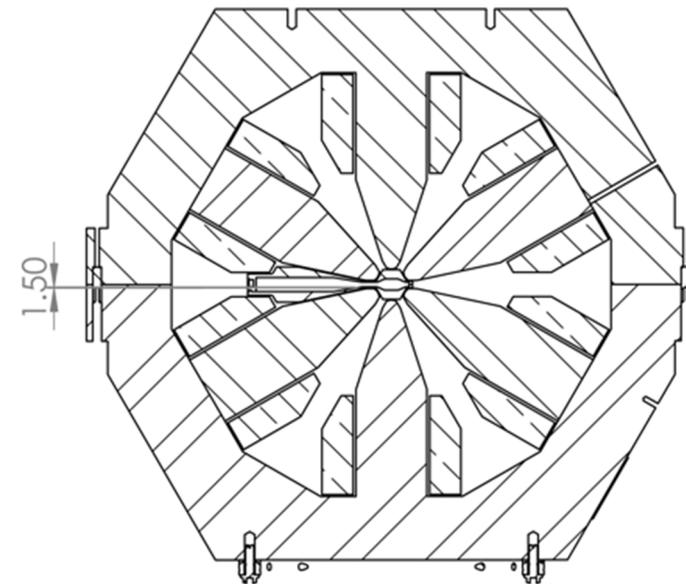
- 50% of main components aim to be manufactured domestically. Especially, Magnets, UHV chambers, and High precision girders.

Space limitation

- Small magnet bore aperture vs BSC >> less chamber thickness & less conductance
- Dense magnets >> no space for pumps and other equipment (bellow, gate valve, etc.)

Impedance

- RF-shield bellow, flange & gasket,



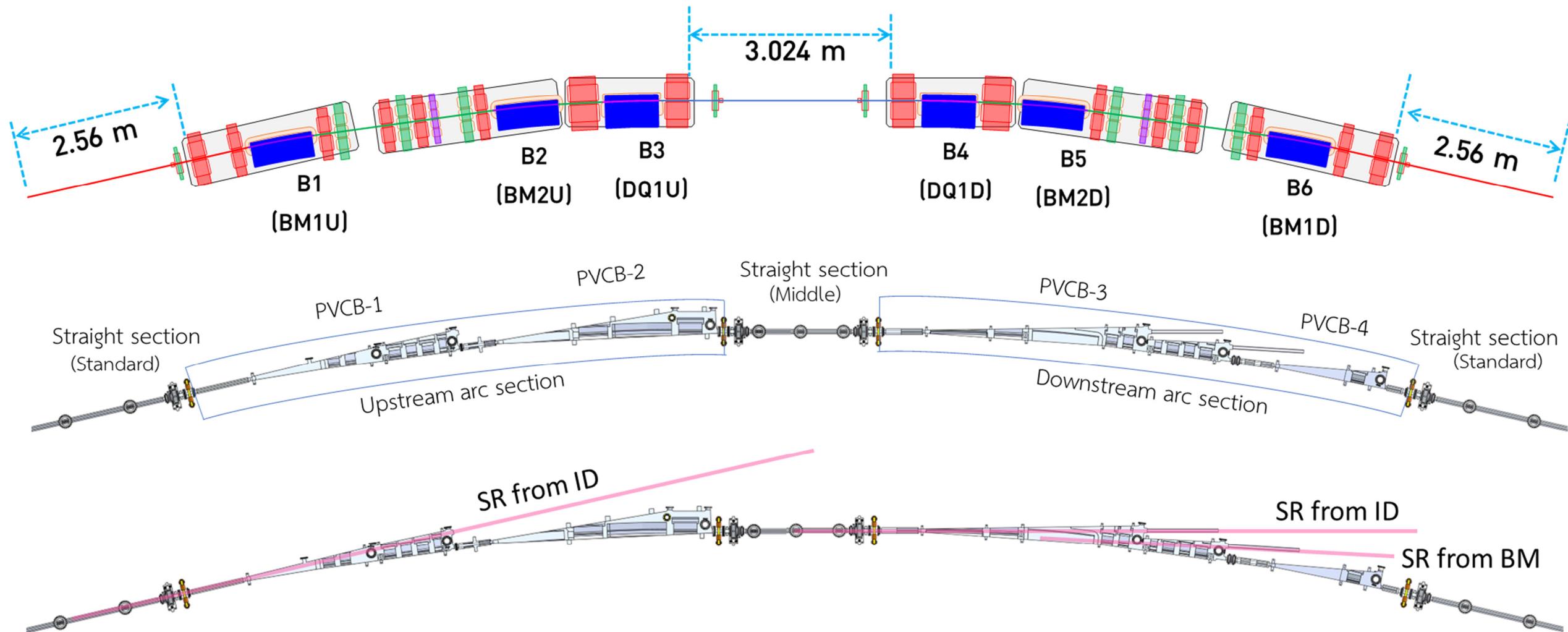
Selection of Vacuum Chamber Material

| Specifics | Aluminium | Stainless Steel | Copper |
|----------------------|---|---|--|
| Initial PSD rate | Low | Low | Low |
| Mechanical strength | Acceptable | Excellent | Good |
| Thermal expansion | Large | Small | Small |
| Thermal conductivity | Excellent | Poor | Excellent |
| Weld ability | Difficult | Excellent | Good |
| Bi-metal flanges | Yes | No | Yes |
| Cooling channels | Extrusion | Brazed | Brazed |
| Fabrication cost | Low | Average | Expensive |
| Precision | Good | Poor | Acceptable |
| Radiation shielding | Poor | Average | Excellent |
| Necessary Tech. R&D | <ol style="list-style-type: none"> Oil-less Machining Precision Welding | <ol style="list-style-type: none"> Copper plating Precision Machining Demagnetization Vacuum firing | <ol style="list-style-type: none"> Clean brazing furnace Extremely high heat load absorber |

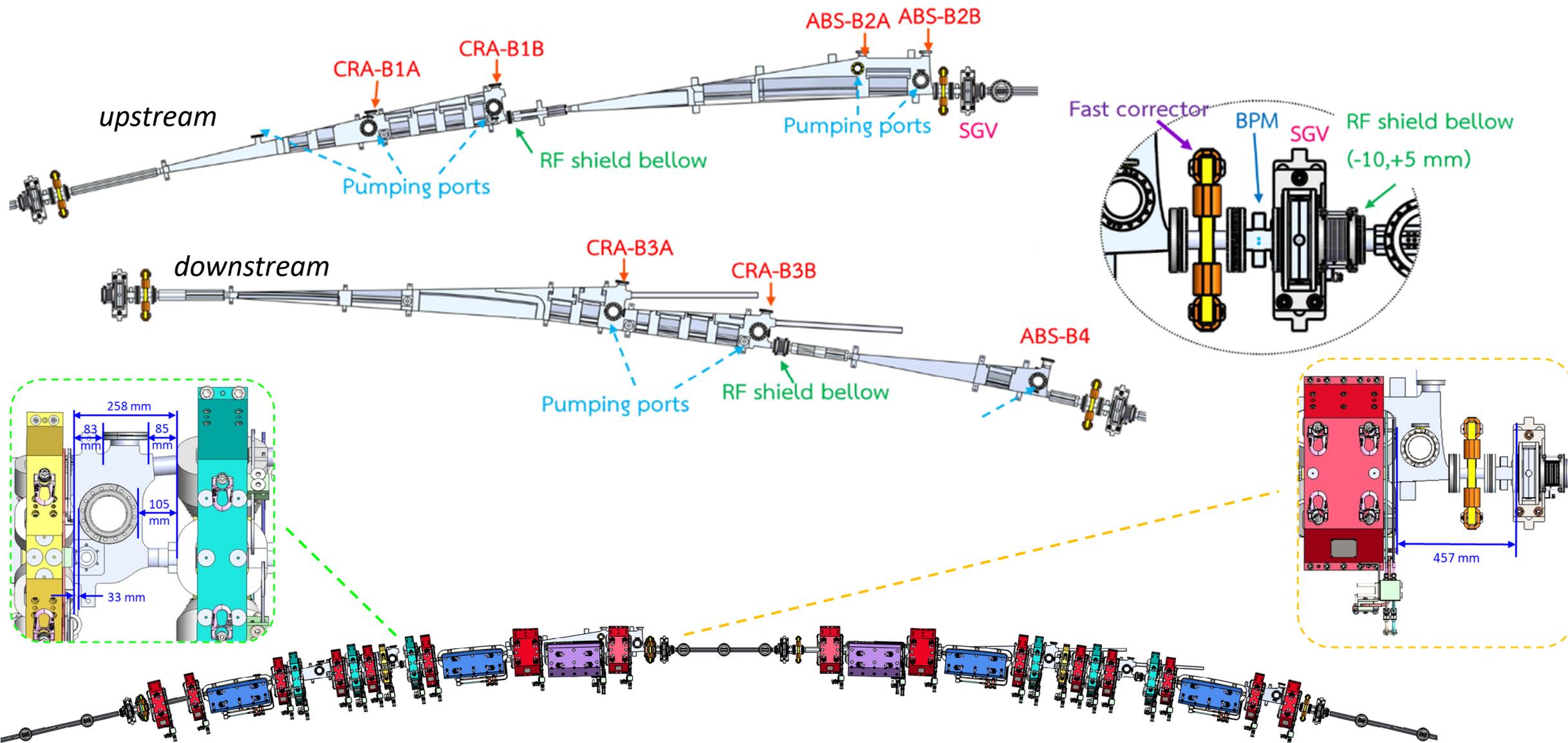
The decision to proceed with aluminum was based on the following factors:

- 1) A short R&D period to complete the copper plating process and quality testing.
- 2) Advice from our advisor, Prof. Chen, especially regarding the welding process.
- 3) The advantages of aluminum, including its lightweight nature, high strength-to-weight ratio, corrosion resistance, thermal conductivity, high-precision machinability, and cost-effectiveness.

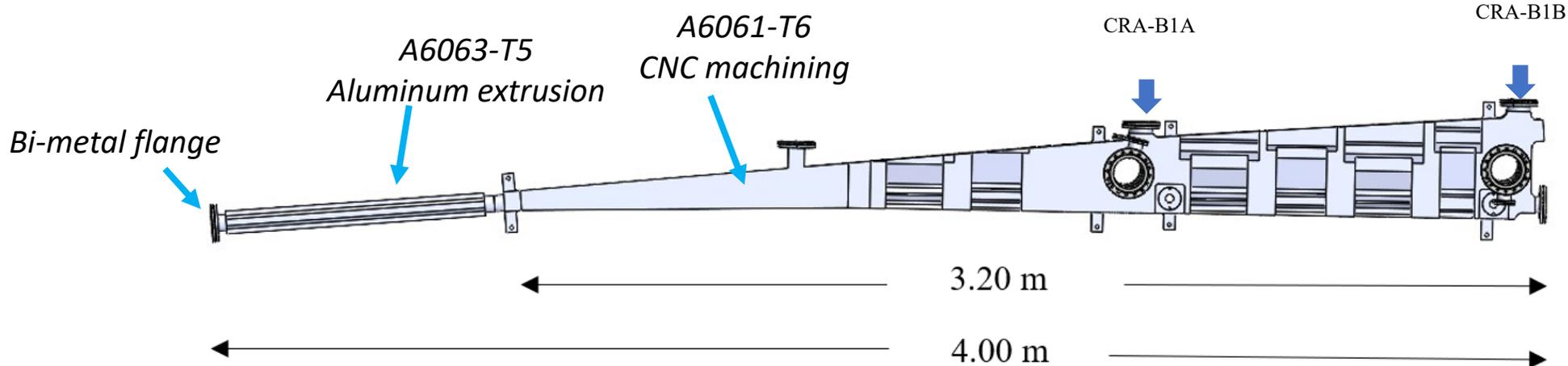
Storage ring: DTBA lattice and chamber sections



Arc section



Bending chamber design



Material properties

| Material property | Al6061-T6 | Al6063-T5 |
|---|-----------|-----------|
| Density (kg/m ³) | 2,700.0 | 2,700.0 |
| Ultimate stress (MPa) | 310.0 | 185.0 |
| Yield stress (MPa) | 276.0 | 145.0 |
| Modulus of elasticity (GPa) | 68.9 | 69.0 |
| Poisson's ratio | 0.33 | 0.33 |
| Coefficient of Thermal Expansion (e-6/°C) | 23.2 | 23.4 |
| Melting point (°C) | 588.0 | 616.0 |

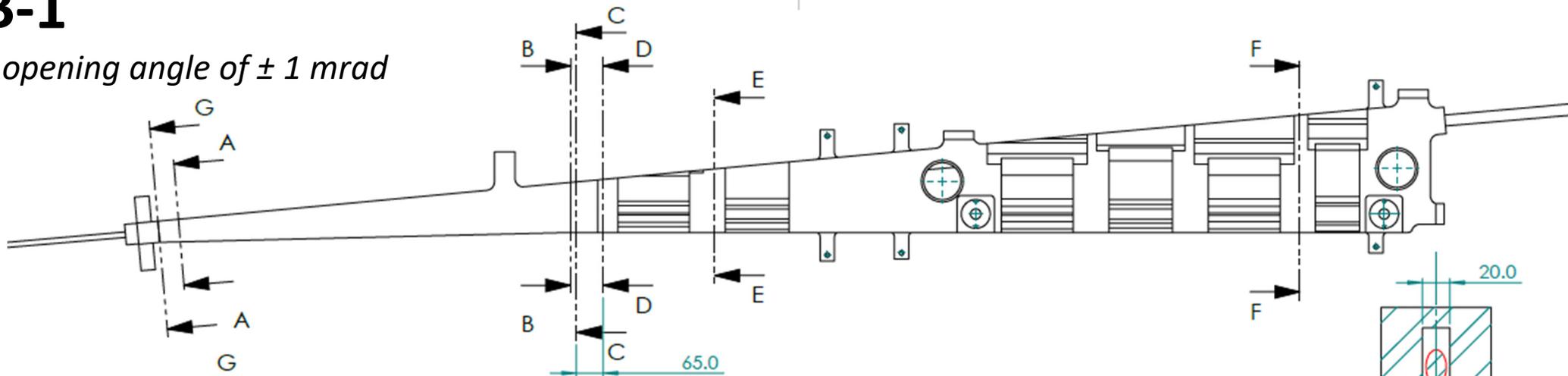
Structural tolerances

| | |
|-------------------------------------|--|
| Total deformation | < 1 mm |
| Longitudinal deformation | < 1 mm |
| Vertical and horizontal deformation | < 0.1 mm (beam duct) < 0.3 mm (antechamber) |
| Safety factor | > 2 |

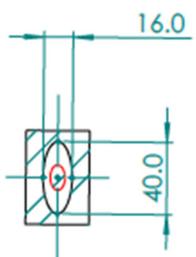
Bending chamber design

PVCB-1

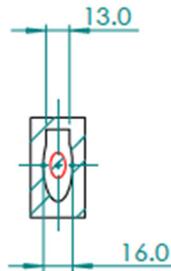
Vertical opening angle of ± 1 mrad



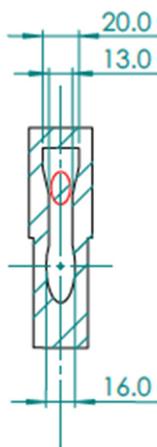
Increase antechamber gap to 13 mm then taper to 6.6 mm



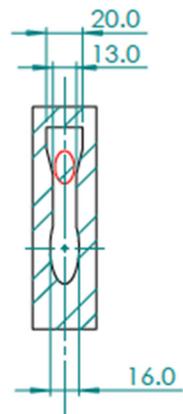
SECTION G-G
SCALE 1 : 3



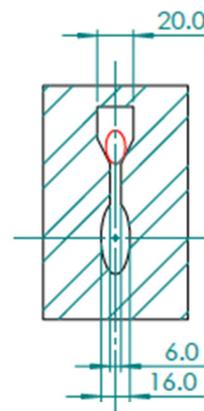
SECTION A-A
SCALE 1 : 3



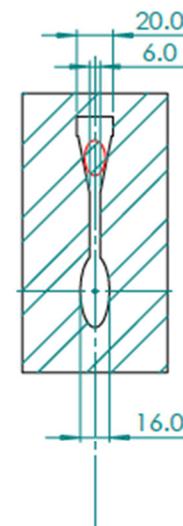
SECTION B-B
SCALE 1 : 3



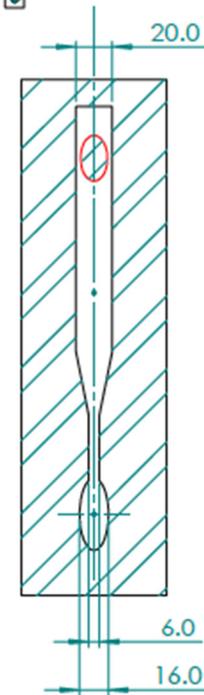
SECTION C-C
SCALE 1 : 3



SECTION D-D
SCALE 1 : 3



SECTION E-E
SCALE 1 : 3



SECTION F-F
SCALE 1 : 3

Chamber structural simulation: PVCB-1

N: Copy of Copy of Automatic+force thick 80 mm
 Static Structural
 Time: 1. s
 6/19/2023 2:16 PM

- A** Standard Earth Gravity: 9806.6 mm/s²
- B** Pressure: 0.10132 MPa
- C** Fixed Support
- D** Displacement
- E** Pump1: 98.1 N
- F** Pump2: 98.1 N
- G** ABS1: 50.059 N
- H** ABS2: 75.075 N
- I** Flange CF114: 12.783 N

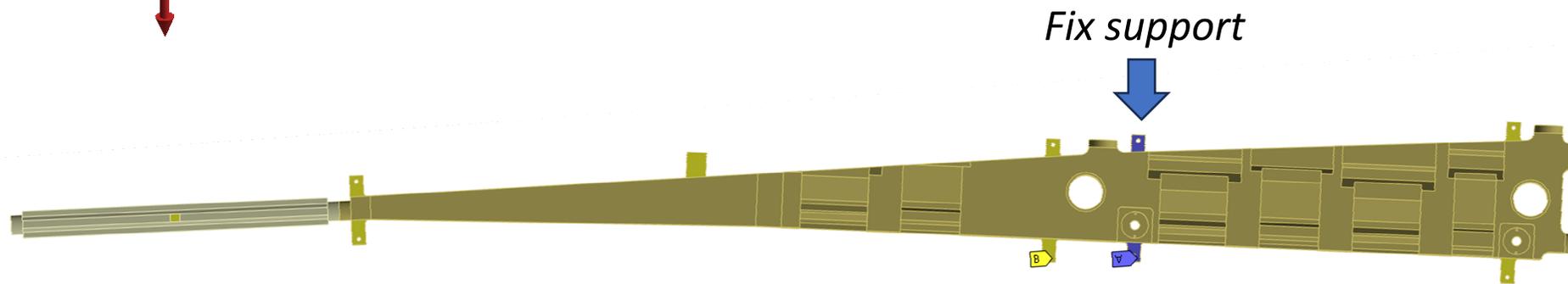


Input parameters

1. Forces due to

- Chamber weight
- Atmospheric pressure
- Pumps
- Photon absorbers

2. Temperature: 35°C



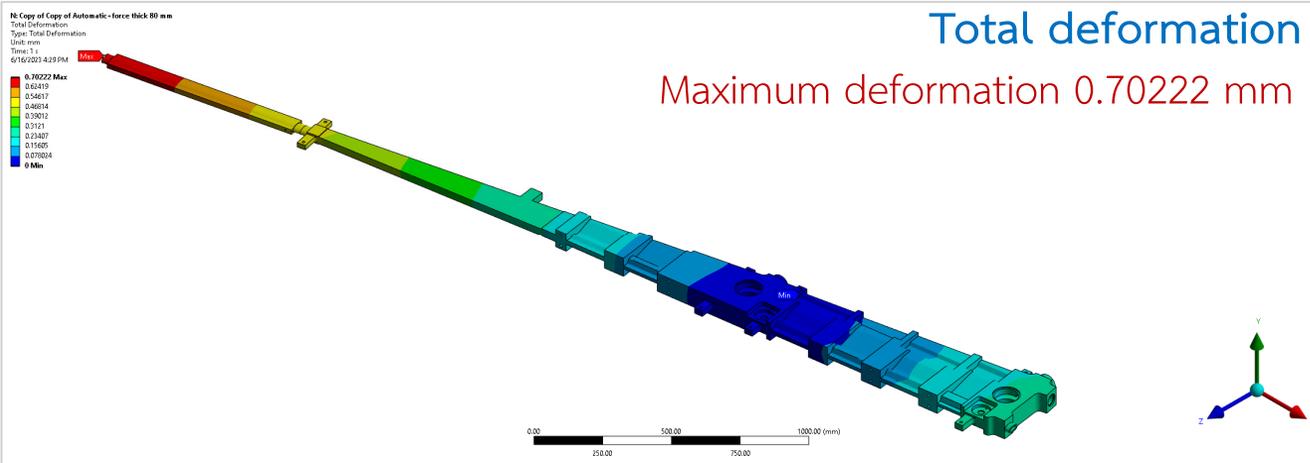
- A** Fixed Support
- B** Displacement

1 fixed support and 4 displacements (The chamber can move freely on longitudinal direction)

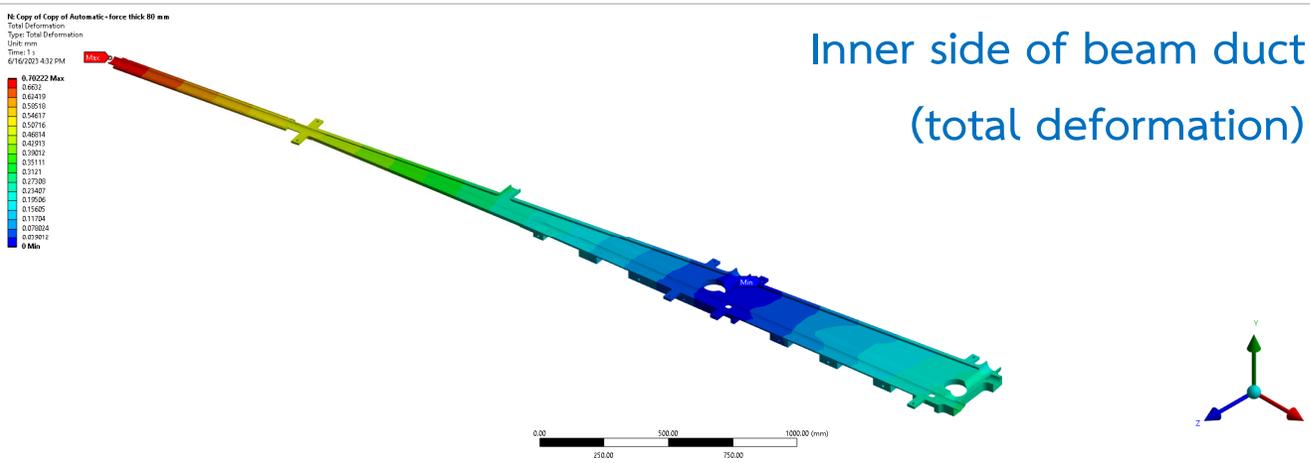
PVCB-1 simulation: deformation

Total deformation

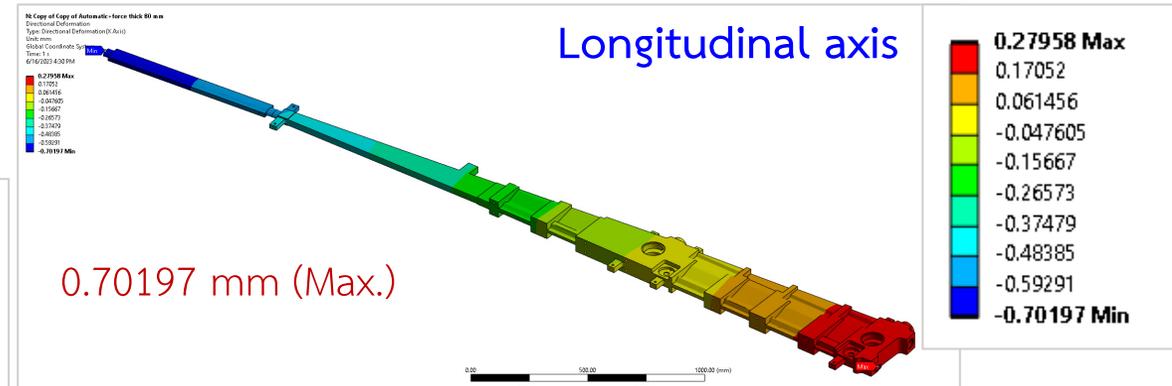
Maximum deformation 0.70222 mm



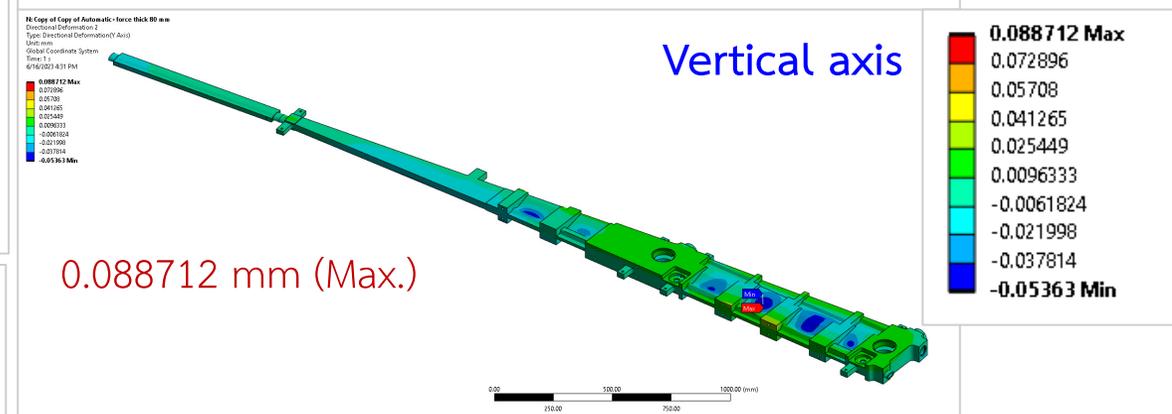
Inner side of beam duct (total deformation)



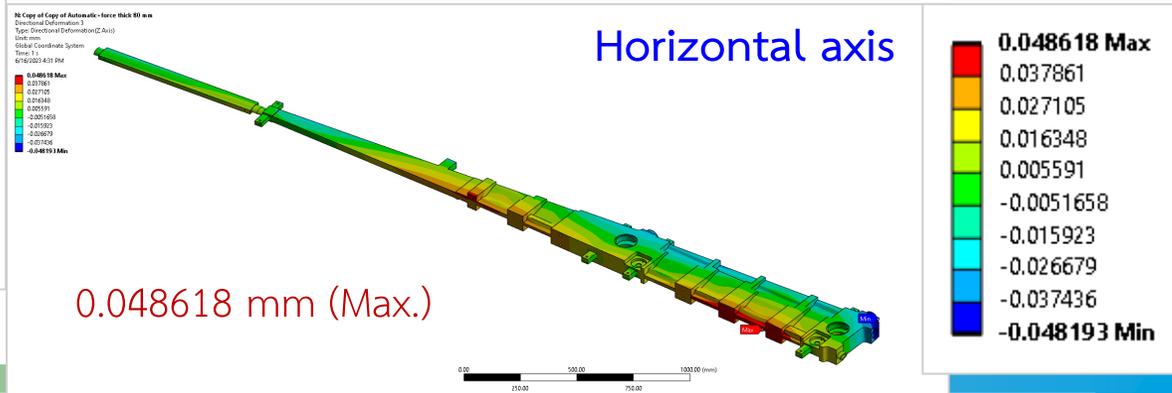
Longitudinal axis



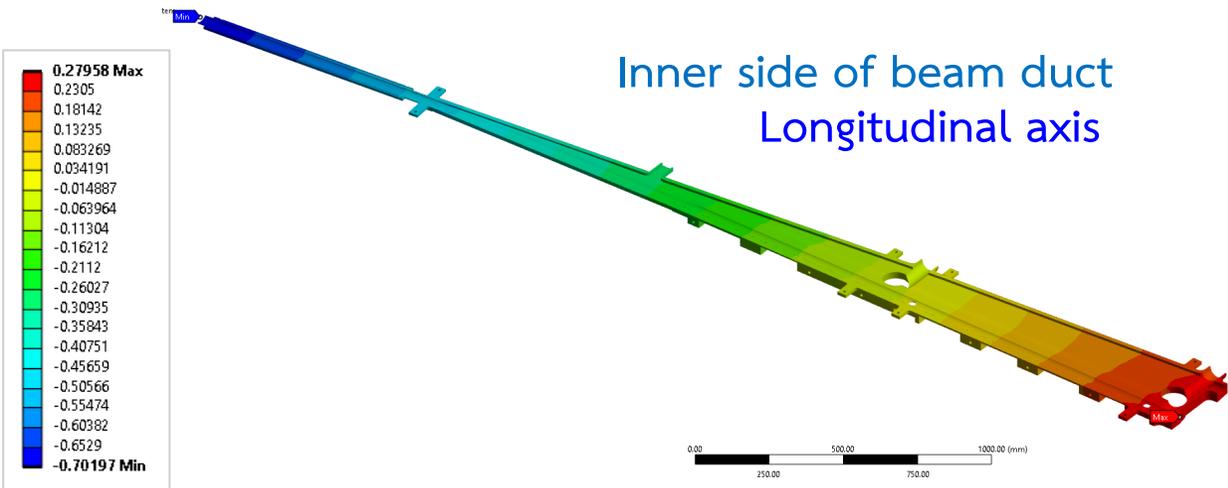
Vertical axis



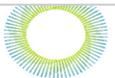
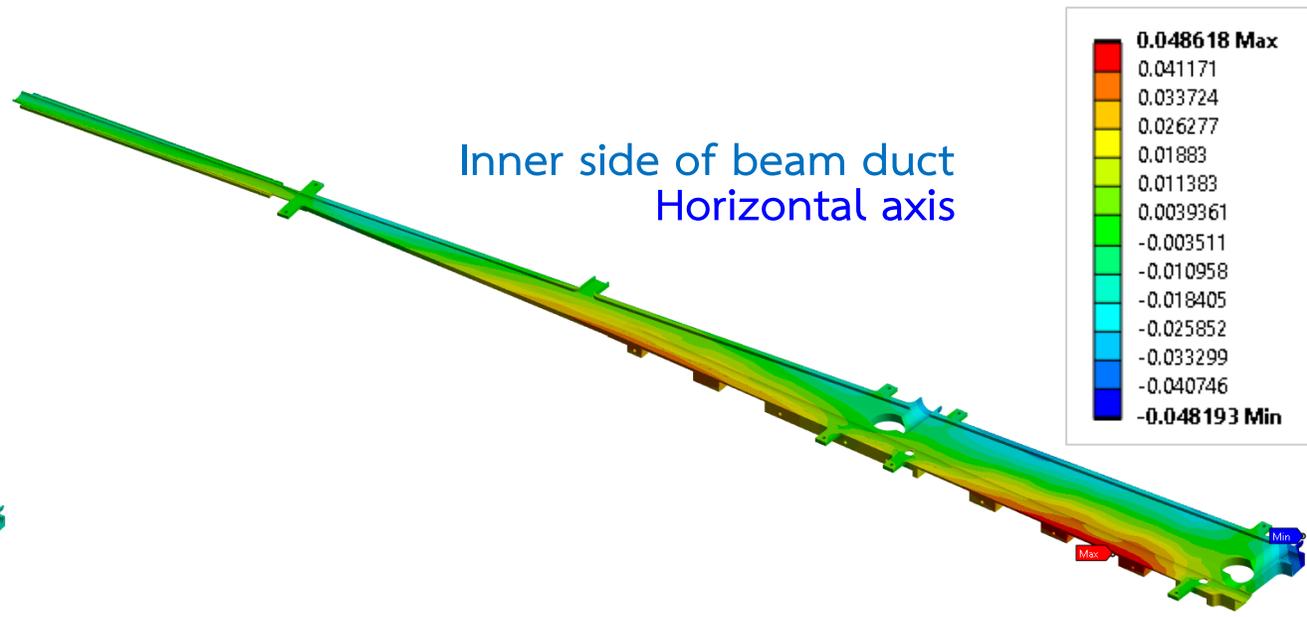
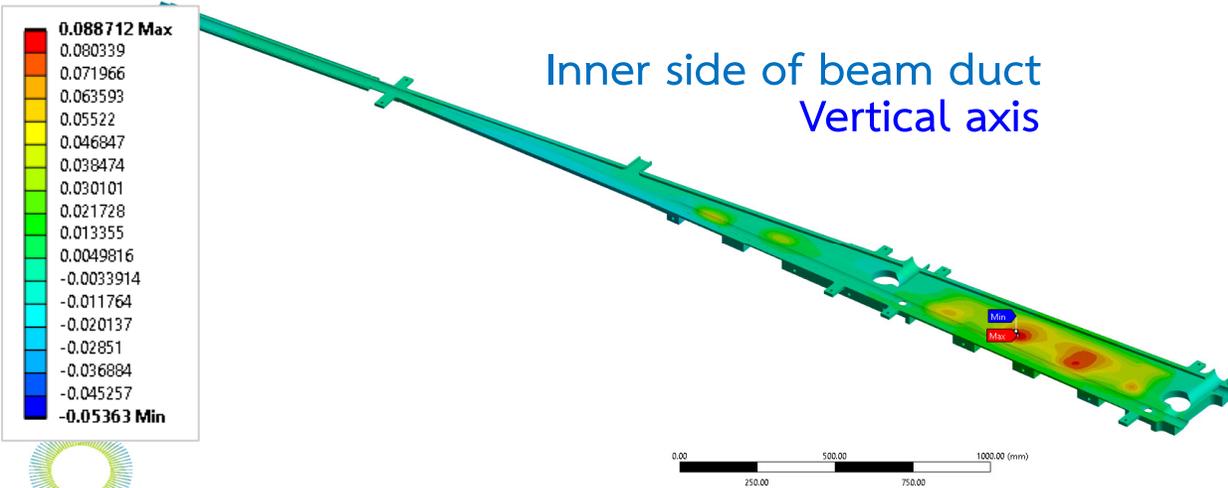
Horizontal axis



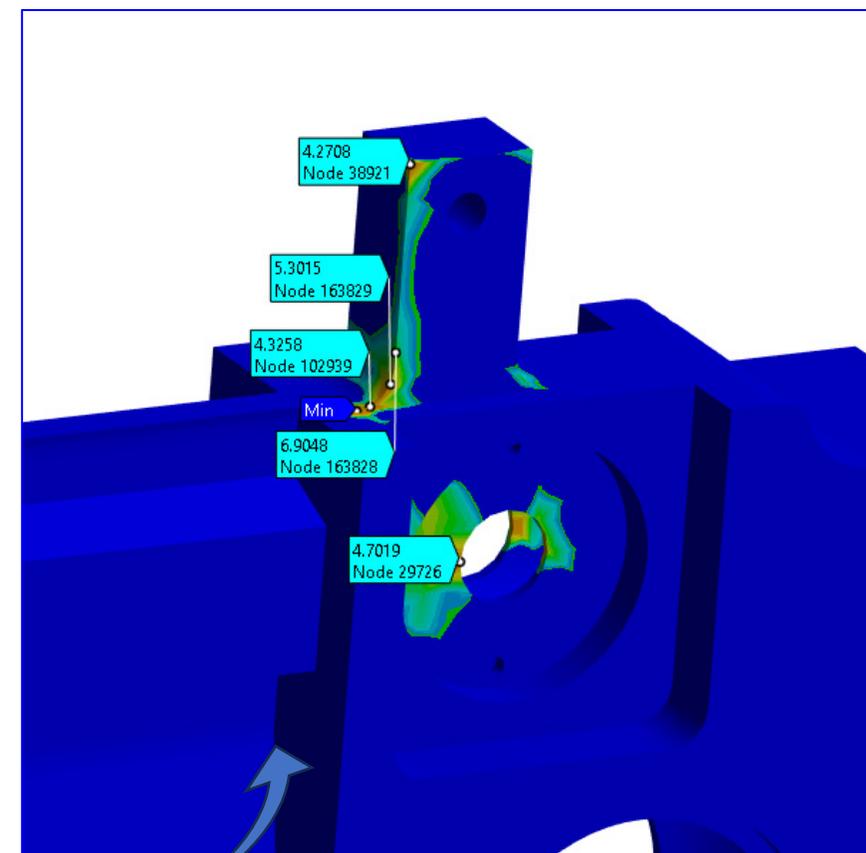
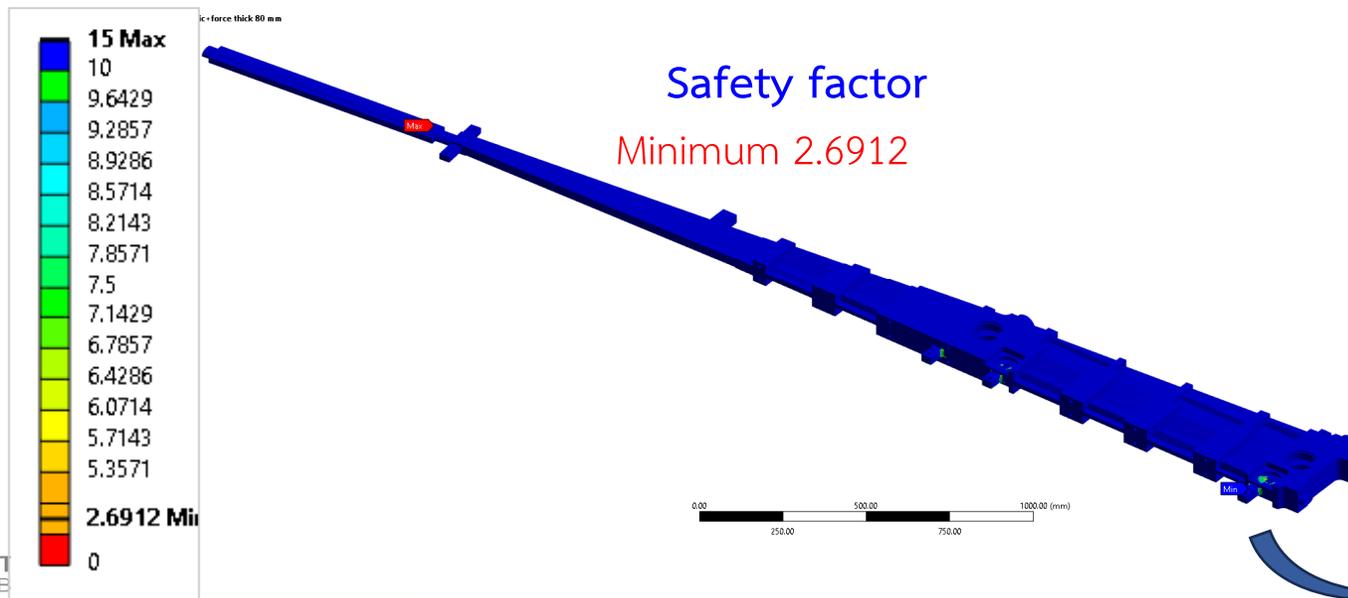
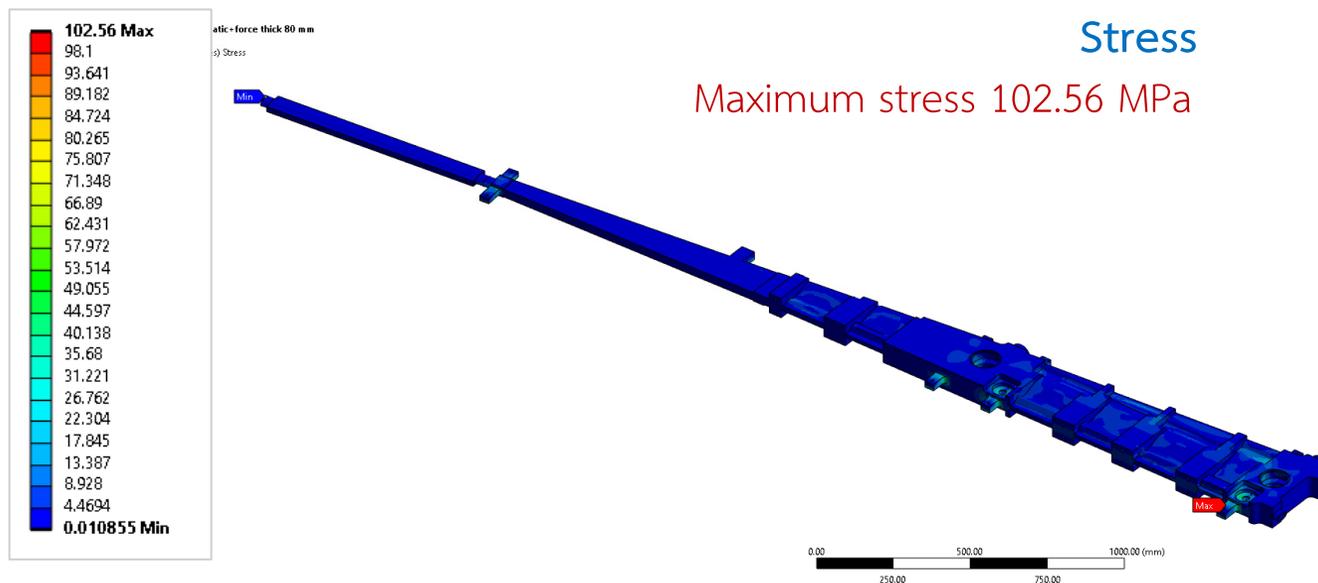
PVCB-1 simulation: deformation



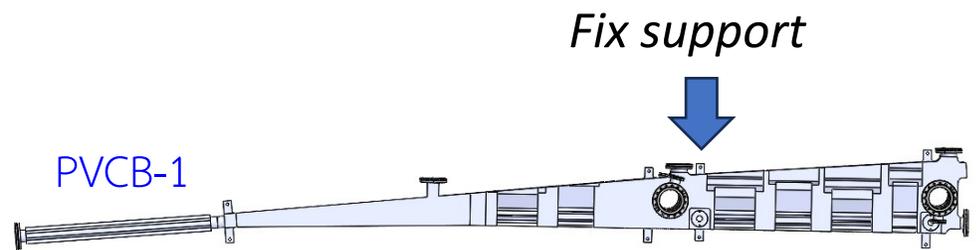
| Simulation result | Max. value |
|---|--------------|
| Total deformation (mm) | 0.70222 |
| Longitudinal directional deformation (mm) | 0.27958 (+) |
| Vertical directional deformation (mm) | 0.088712 (-) |
| Horizontal directional deformation (mm) | 0.048618 (+) |



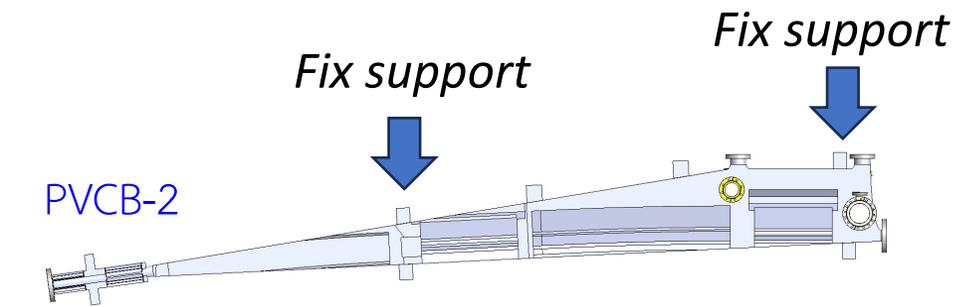
PVCB-1 simulation: stress and safety factor



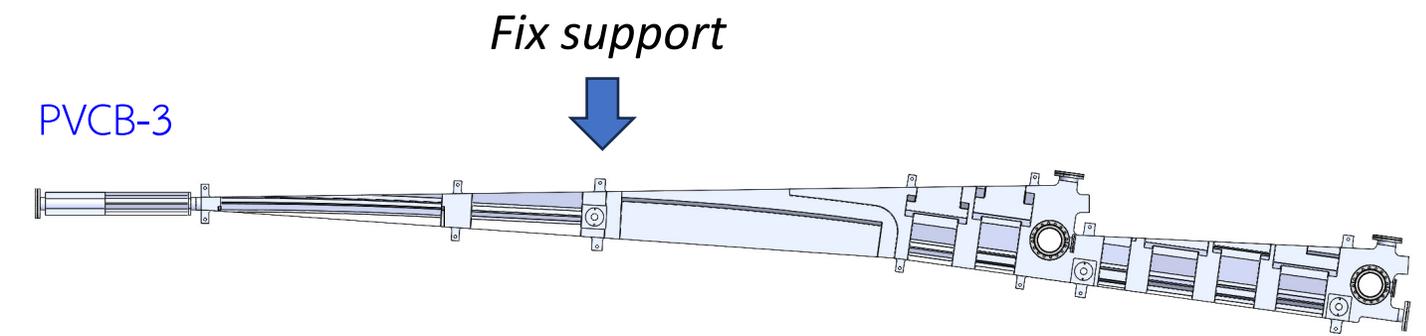
Chamber structural simulation result



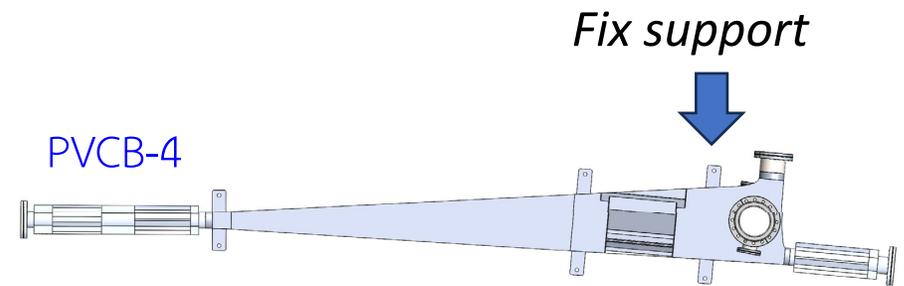
PVCB-1



PVCB-2



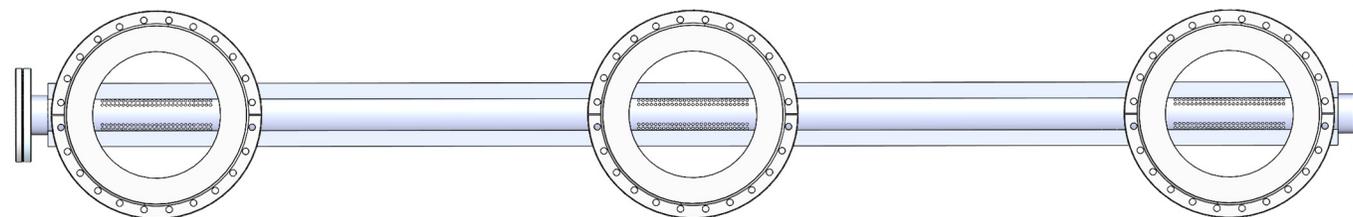
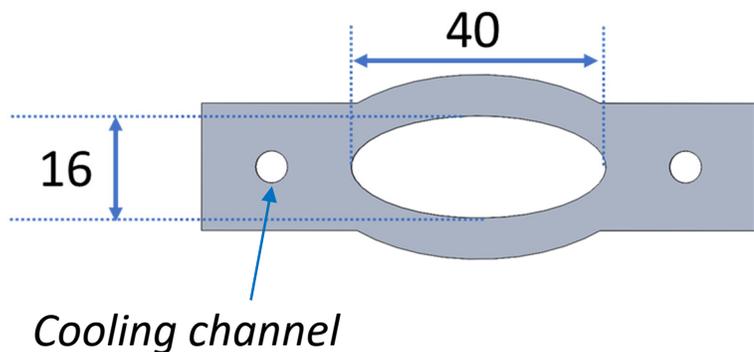
PVCB-3



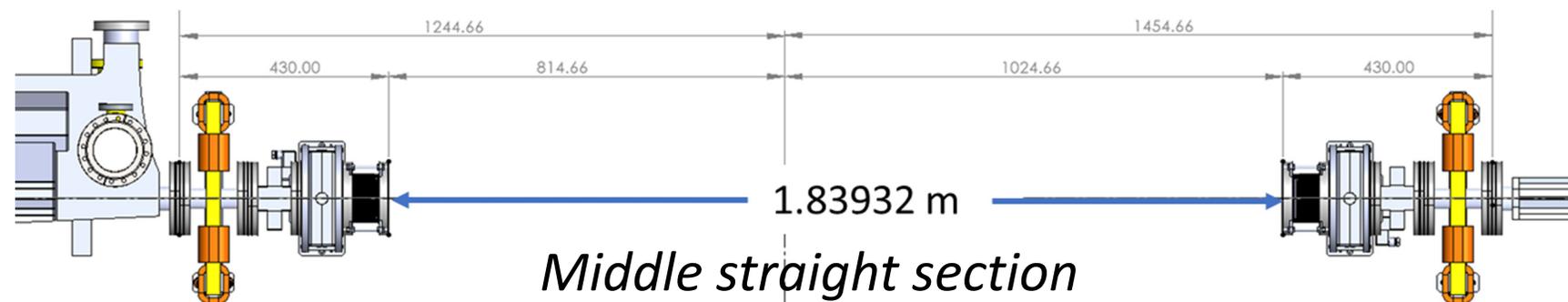
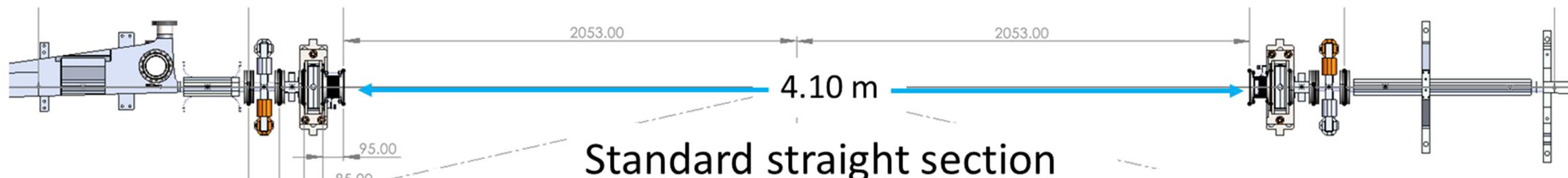
PVCB-4

| Simulation result | PVCB-1 | PVCB-2 | PVCB-3 | PVCB-4 |
|--|-----------|-----------|-----------|-----------|
| Max. Equivalent stress (MPa) | 102.56 | 104.22 | 124.91 | 99.381 |
| Min. Safety factor | 2.7 | 2.2 | 2.2 | 2.5 |
| Max. Total deformation (mm) | 0.70 | 0.22 | 0.75 | 0.44 |
| Max. Longitudinal directional deformation (mm) | 0.28 (+) | 0.216 (-) | 0.750 (+) | 0.444 (-) |
| Max. Vertical directional deformation (mm) | 0.089 (-) | 0.078(-) | 0.113 (-) | 0.065 (-) |
| Max. Horizontal directional deformation (mm) | 0.049 (+) | 0.045(-) | 0.076 (-) | 0.055 (+) |

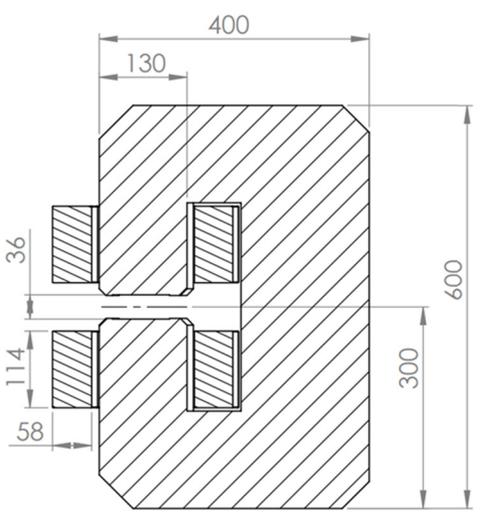
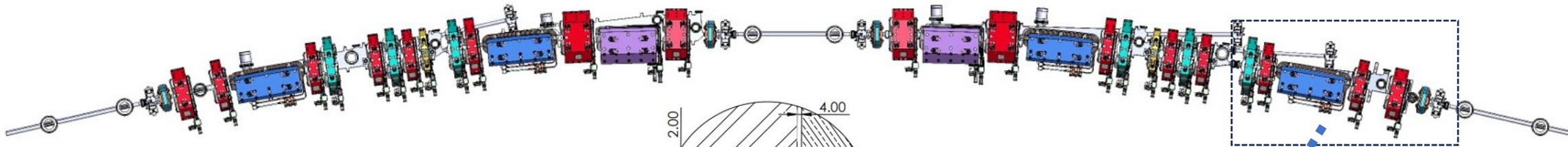
Straight section



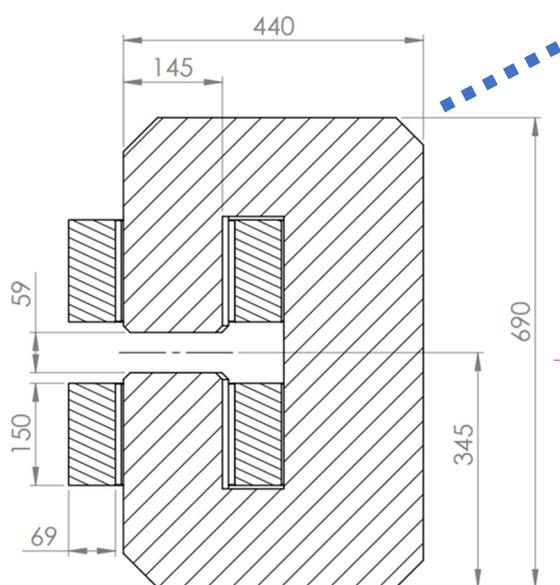
Aluminum vacuum chambers in straight section have been designed based on TPS model aiming for beam cleaning



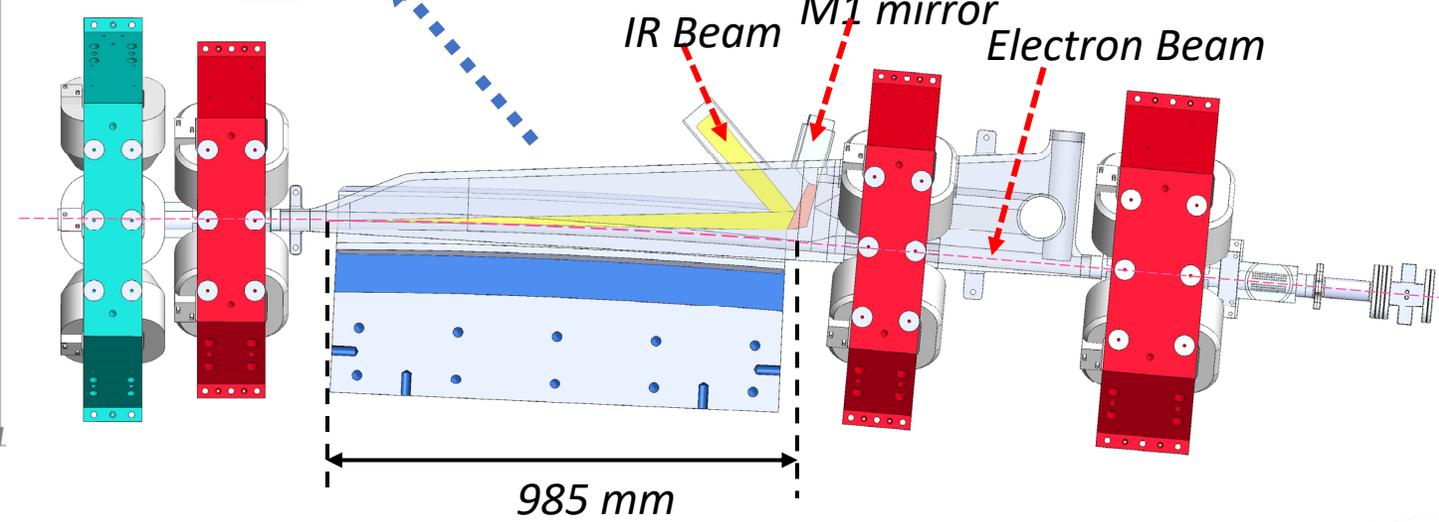
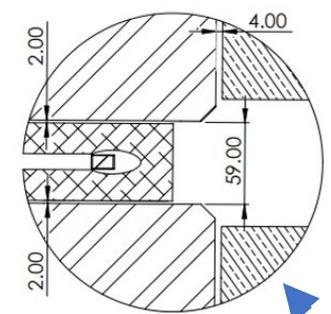
Bending chamber for IR beamline



36 mm dipole



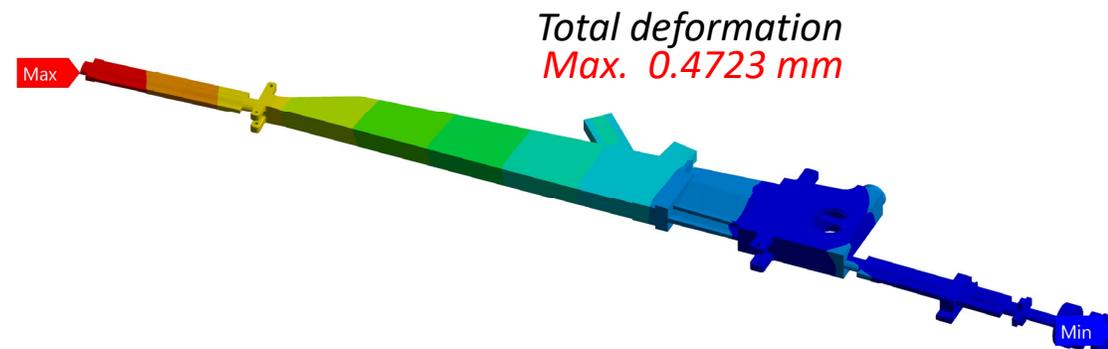
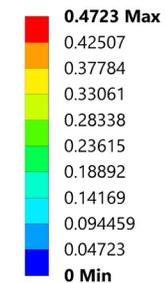
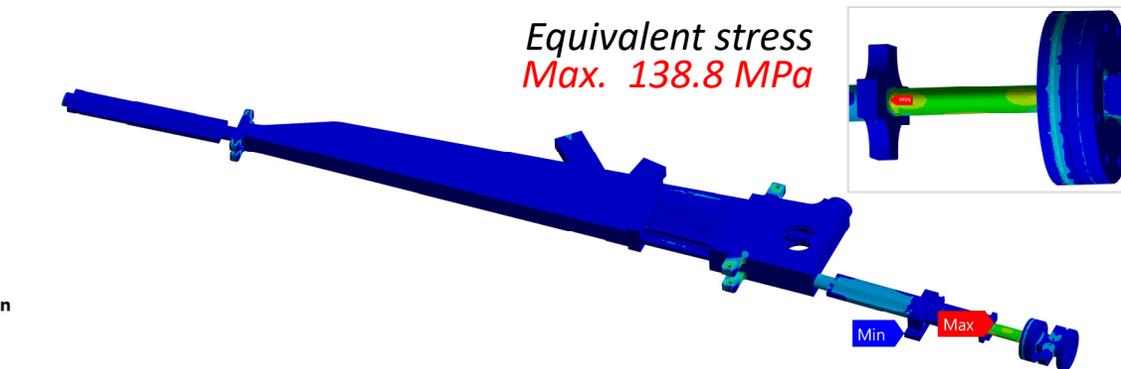
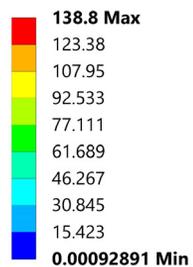
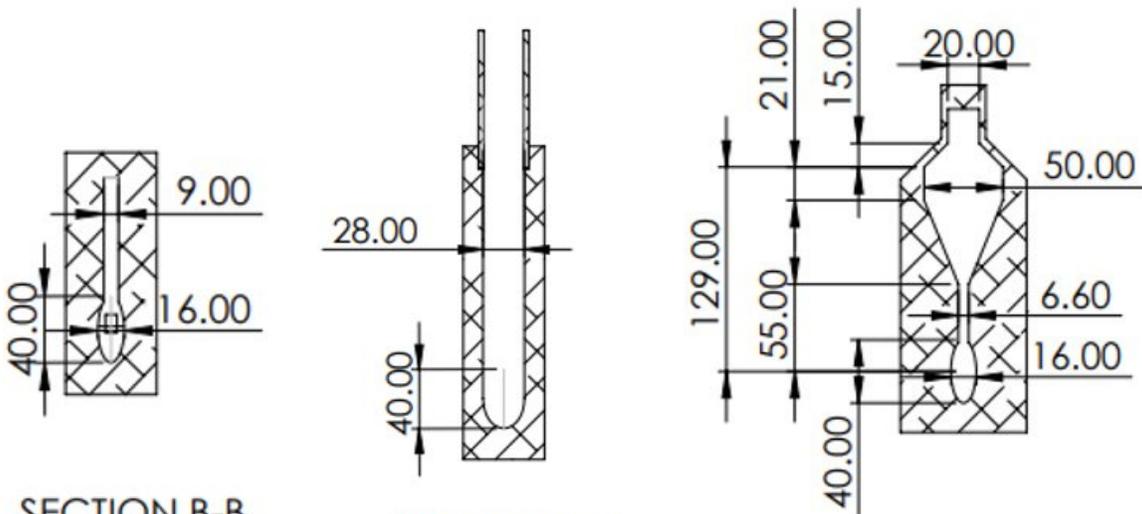
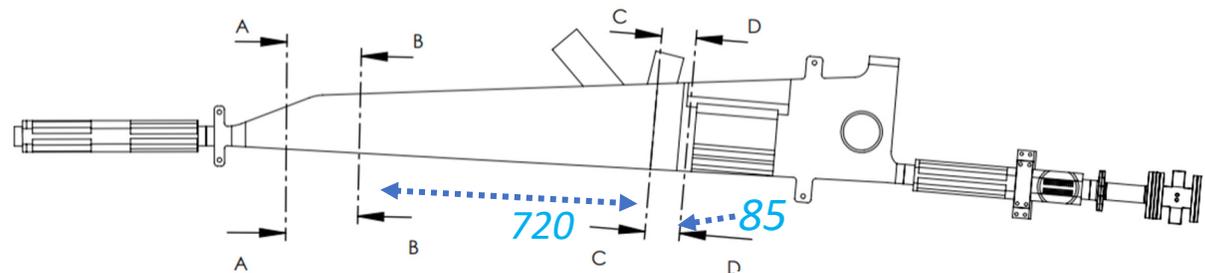
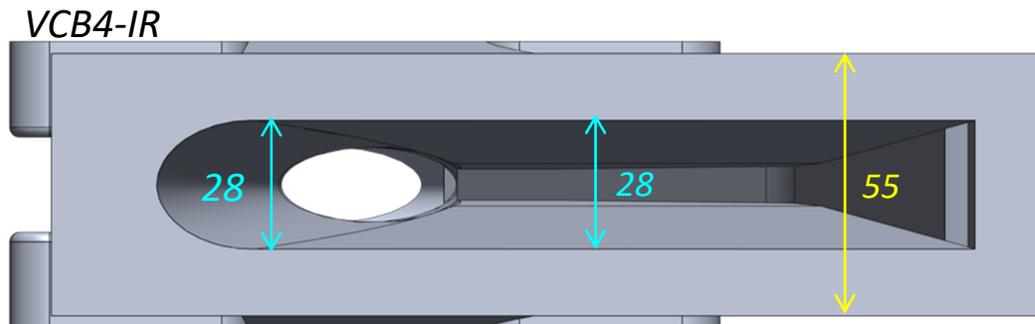
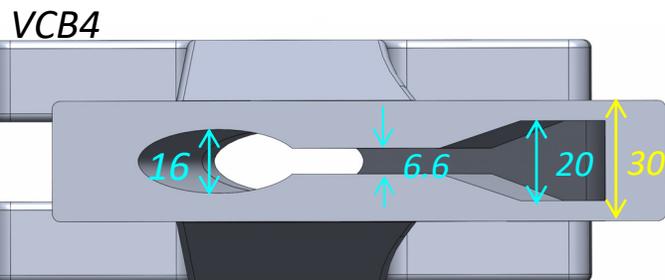
59 mm dipole



IR Beam
M1 mirror
Electron Beam

985 mm

Bending chamber for IR Beamline

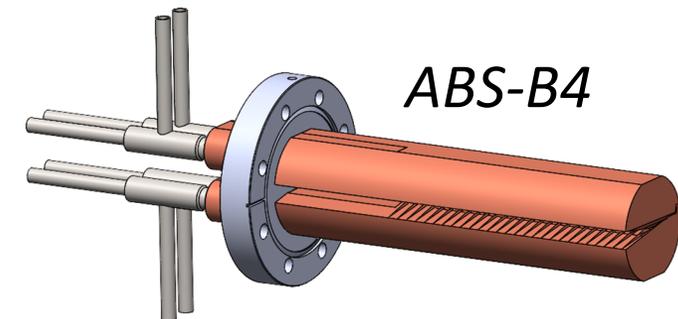
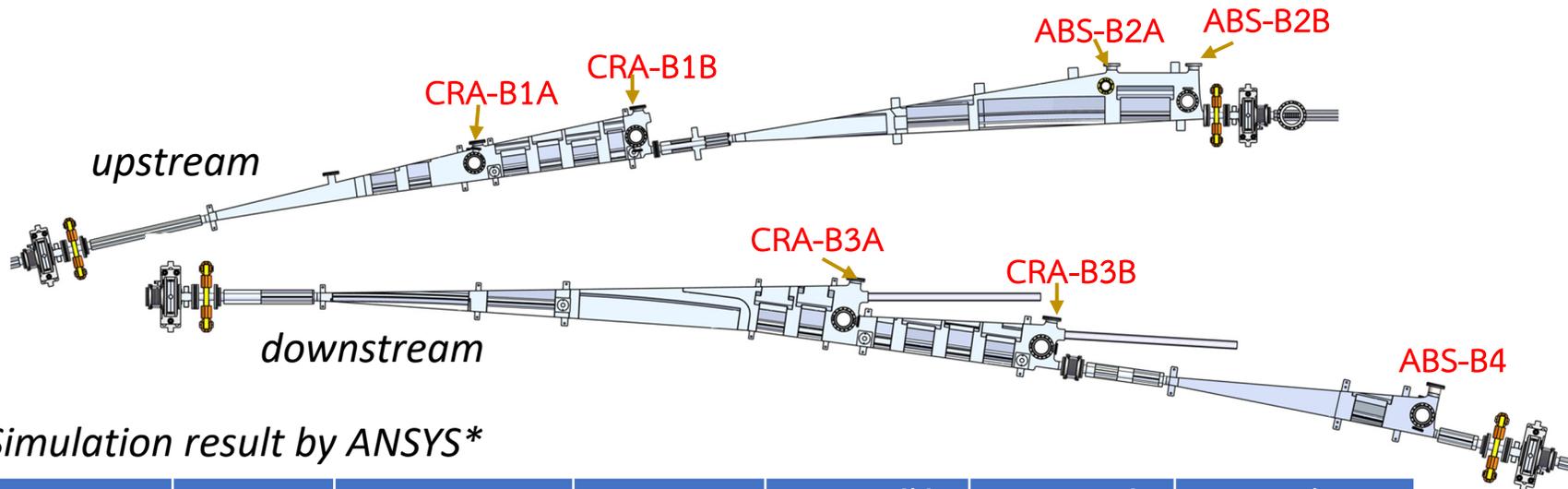


SECTION B-B

SECTION C-C

SECTION D-D

Photon absorbers



Flat



V-shape fin



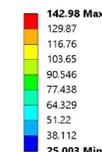
Triangular fin



Rectangular fin



A: Steady-State Thermal
ABS Temperature
Type: Temperature
Unit: °C
Time: 1 s
7/12/2023 11:41 AM



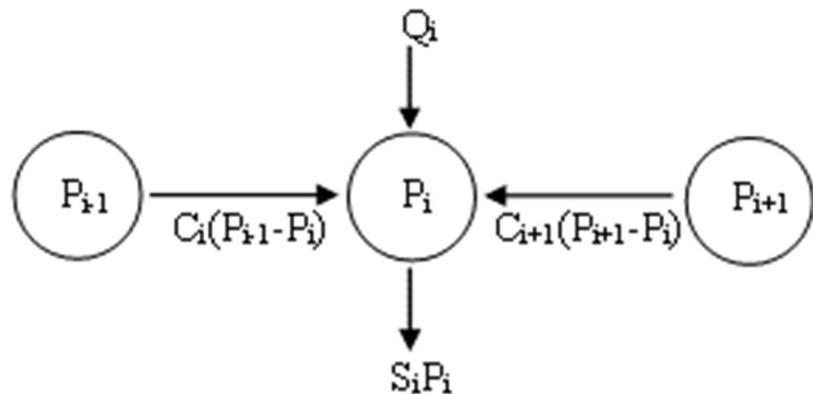
Temperature contours of ABS-B4

Simulation result by ANSYS*

| Absorbers | Total heat load (kW) | Max power density (W/mm ²) | model | Max. solid temperature (°C) | Max. Total Deformation (mm) | Von-Mises stress (MPa) |
|-----------|----------------------|--|-------------|-----------------------------|-----------------------------|------------------------|
| CRA-B1A | 1.30 | 57.53 | Rectangular | 132.75 | 0.053 | 64.059 |
| CRA-B1B | 3.52 | 32.94 | V-shape | 130.99 | 0.248 | 52.542 |
| ABS-B2A | 1.36 | 35.05 | Flat | 134.19 | 0.064 | 75.103 |
| ABS-B2B | 5.35 | 133.95 | Rectangular | 121.22 | 0.260 | 34.337 |
| CRA-B3A | 2.39 | 82.14 | Flat | 120.08 | 0.169 | 57.660 |
| CRA-B3B | 4.54 | 34.83 | Rectangular | 95.47 | 0.195 | 56.903 |
| ABS-B4 | 4.16 | 181.19 | Triangular | 145.31 | 0.150 | 99.137 |

* The convection heat transfer coefficient of 10,000 W/m²°C
The power calculated using current of 600mA

Pressure profile – Original design



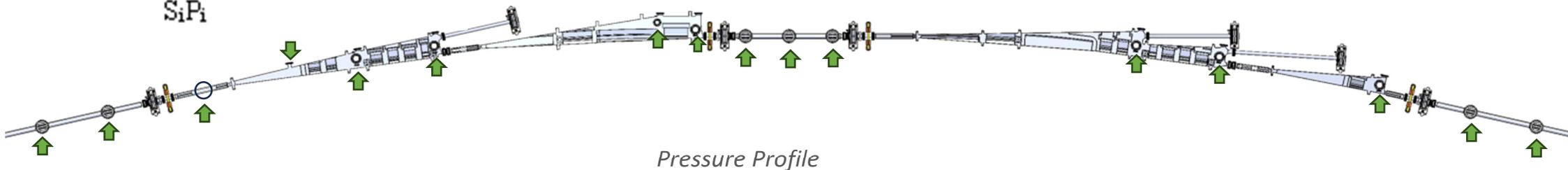
$$S_i P_i = Q_i + C_i (P_{i-1} - P_i) + C_{i+1} (P_{i+1} - P_i).$$

S : pumping speed (l/s),

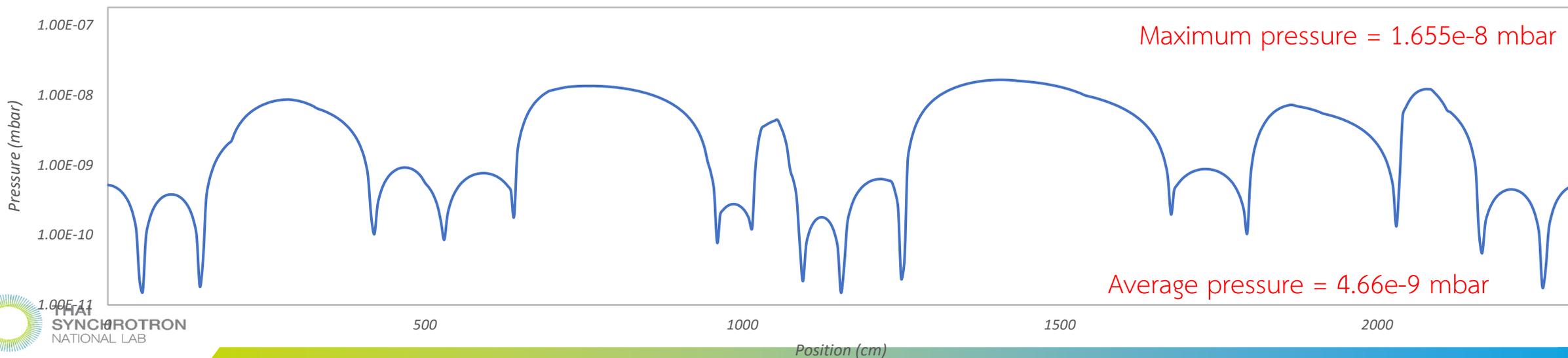
P : pressure (mbar),

Q : outgassing rates = photon flux \times PSD yield ($\eta \approx 1e-6$ mol./ph),

C : conductance ($C_{Bending} \approx 80$ l/s , $C_{Straight} \approx 20$ l/s).

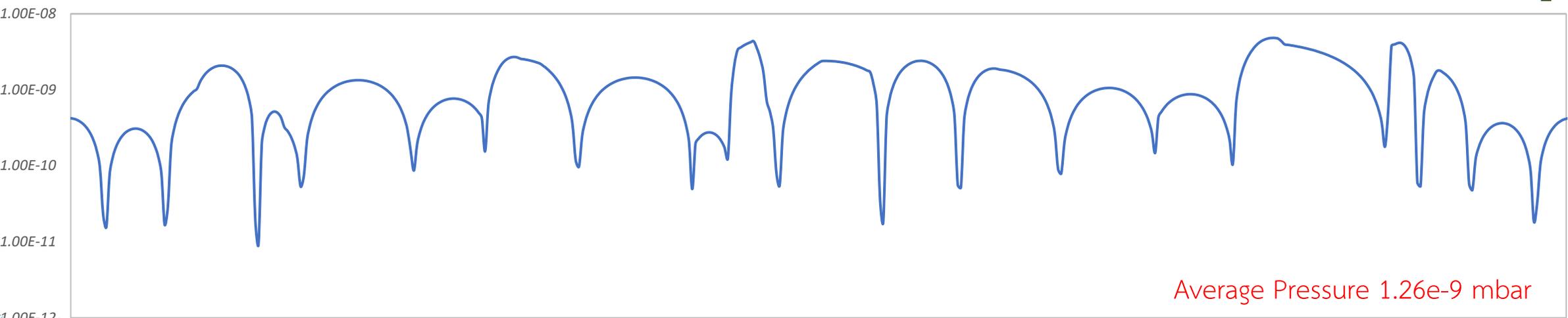
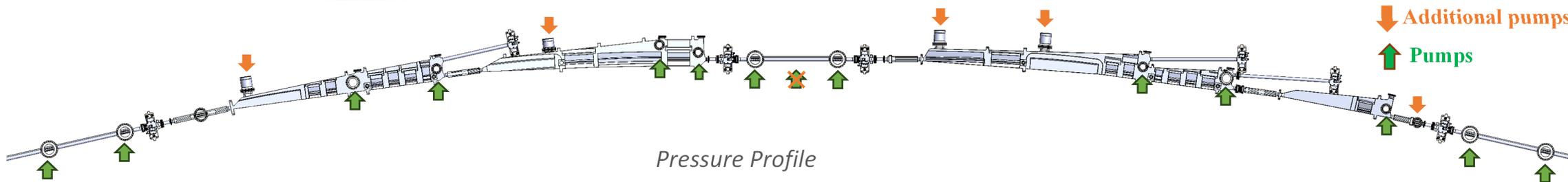
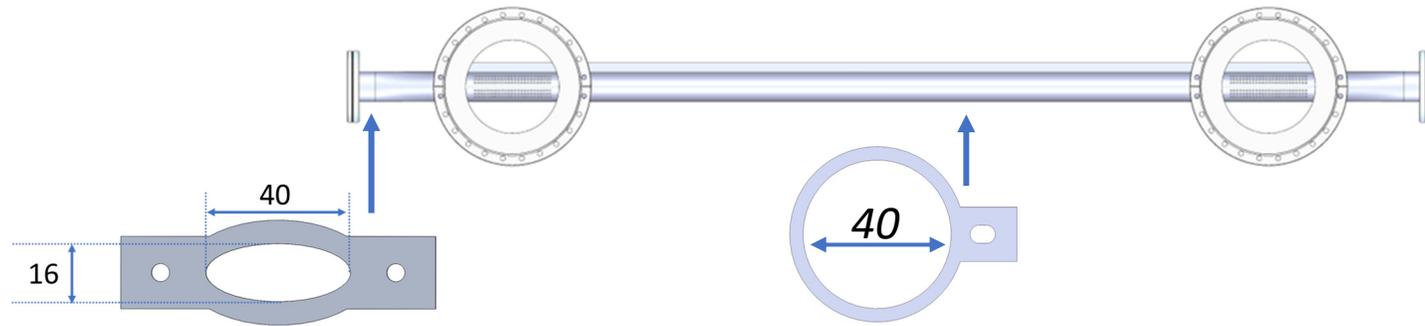
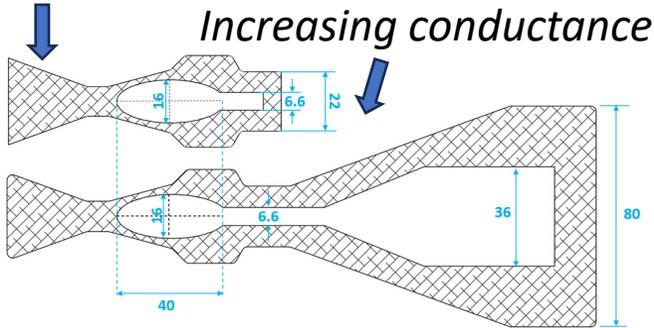


Pressure Profile



Pressure profile – Improved design

Original design



Vacuum Chamber Prototype for Storage Ring

SUS316L vacuum chamber prototype:

- *Frist prototype was development.*
- *UHV performance test was done.*
- *Copper plating inside the chamber was preliminary tested.*



SUS316L chamber and copper plating is not continuously developed.

Aluminum vacuum chamber prototype:

- *Frist prototype was developed.*
- *Preliminary vacuum leak was check and small leakage was found with leak rate 2.5×10^{-7} mbar·l/s.*



- *Leakage was successfully fixed, leak rate better than 5.0×10^{-9} mbar·l/s*
- *UHV performance test was done.*



Infrastructure and technology development

Aluminum welding

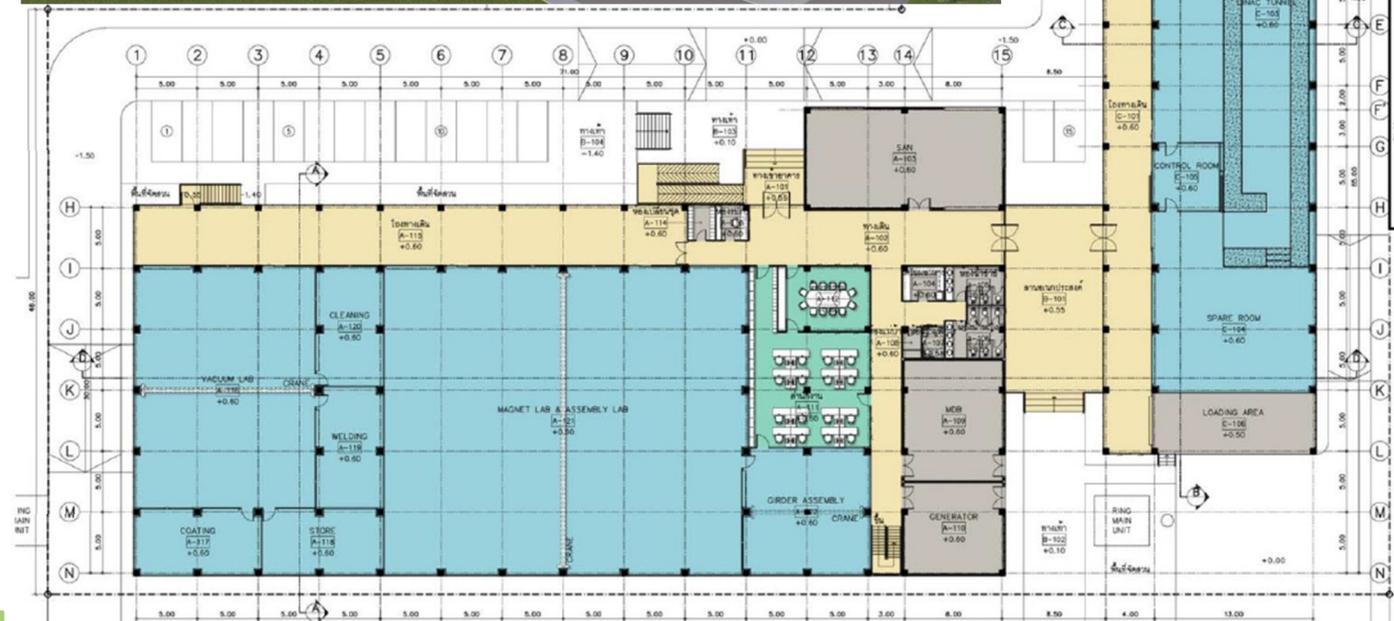
- Technician's welding skill.
- Develop welding machine



Welding practicing



Pilot plant



Conclusion

- Siam Photon Source II (SPS-II) is Thailand's first 4th generation synchrotron light source. It will provide high-energy and high-brightness synchrotron radiation for both academic and industrial research.
- The vacuum system is expected to play a crucial role in enhancing the country's manufacturing capability. Most of the main components in the system are planned to be domestically fabricated through technology transfer. The project will prioritize local economic advantages by utilizing conventional vacuum technology.
- Conventional technology without NEG coating presents several challenges, including limited space for pumps, absorbers, and beam position monitors (BPMs), which can result in the sacrifice of straight section length.
- The bulky chambers require optimization of their thickness to achieve the best strength.
- Prototypes of vacuum chambers have been created to assess local manufacturing capabilities and pinpoint areas for improvement.
- High-precision machining, welding, and surface treatment techniques, such as oil-less machining and chemical cleaning, are the critical technologies that must be developed to meet the project's requirements.
- Two welding technicians have received training, and a pilot plant has been constructed, which includes clean rooms for cleaning, welding, and assembly.



THANK YOU

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THAI
SYNCHROTRON
NATIONAL LAB

Orayanee Seegauncha
Narongsak Sonsuphap
Amphawan Wandu
Sireegorn Sumklang

